

Interactive comment on “Offshore and onshore ground-generation airborne wind energy power curve characterization” by Markus Sommerfeld et al.

Anonymous Referee #2

Received and published: 26 January 2021

5: An universal -> A universal

8: annual energy prediction (AEP) -> production

249: I'm curious about how pressure & density vary with stable vs. unstable conditions and how much that affects power.

271: Why is a reel-out to reel-in ratio used? Is this a combination of a motor torque constraint and the lift during reel-in and reel-out?

279: Assumed lift and drag on reel-in and reel-out should be included here.

280: Was a power constraint used? It's implied in other places.

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357: I'd address elevation angle here; based on figure 10, it looks like the optimizer found a common optimal elevation angle for several of the cases, which links tether length and altitude. Vander Lind 2013 calculated an optimal elevation angle for fly-gen systems assuming an exponential wind profile; I'm curious how close this elevation angle is.

398: Missing a U^3 ?

440: I_{path} and A_{swept} aren't in table 3

459: The fit for c_p is a function of c_{wing} (and because AR is constant, a function of A_{swept}) so it's not non-dimensional and it's not clear how generalizable it is (changes in AR or L/D). I'm curious about whether another definition of c_p may also be comparable to conventional wind turbines but work better. The Loyd paper (see eqs. 1 and 16) shows a limit on a c_p ($4/27 CL^3/CD^2$) defined by wing area. What does your data show for a c_p defined by A_{wing} ? Or if you express c_p as a function of L/D or CL^3/CD^2 ?

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